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1 **Isokinetic Ankle Eversion and Inversion Strength Profiling of Female Ballet Dancers**

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51 **Abstract**

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Ankle injuries are highly prevalent in ballet, with strength highlighted as a primary risk factor. To profile ankle strength, fourteen female ballet dancers (age: 19.29 ± 1.59 years) completed an isokinetic testing protocol comprising concentric eversion (CON_{EV}) and inversion (CON_{INV}), and, eccentric inversion (ECC_{INV}) trials at four angular velocities ($30^{\circ}\cdot s^{-1}$, $60^{\circ}\cdot s^{-1}$, $90^{\circ}\cdot s^{-1}$, $120^{\circ}\cdot s^{-1}$) for both the dominant and non-dominant limb. In addition to Peak Torque (PT) and the corresponding Dynamic Control Ratios (DCRs), angle-specific derivatives of strength (AST) and Functional Range (FR) were calculated. There was no evidence of any significant bilateral strength asymmetry ($p = 0.90$) across all metrics, and no significant interactions with limb and contraction mode or velocity. A significant main effect for contraction mode ($p = 0.001$) highlighted greater ECC_{INV} – which was maintained with increasing isokinetic velocity – in contrast to reductions in CON_{EV} and CON_{INV} strength. Specifically, dancers are ECC_{INV} dominant at angular velocities greater than $60^{\circ}\cdot s^{-1}$, which is likely to be characteristic of most functional tasks. The lack of bilateral asymmetry may be attributed to dance training interventions that facilitate bilateral development, but ipsilateral mode and velocity specific asymmetries have implications for injury risk and the training needs of female ballet dancers.

Key words: Dancers, Female athletes, Ankle injury, Joint strength, Isokinetic dynamometer.

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1. Introduction

Ballet is a compound of artistry and athleticism demanding an intermittent locomotor profile of lower intensity activity interspersed with multiple, explosive jump-landing manoeuvres (Hincapie, Morton & Cassidy, 2008). The mechanical complexity and rigorous nature of ballet is routinely associated with injury risk, reported to affect between 13%-100% of dancers (Comin, Cook, Malliaras, McCormack, Calleja, Clarke & Connell, 2013; Negus, Hopper & Briffa, 2005). Injury incidence rates have been shown to range between 0.4-4.8 per 1000 hours of dance exposure (Smith, Gerrie, Varner, McCulloch, Lintner & Harris, 2015), with comparable trends for gender and training status. Female and male amateur dancers sustain 1.77 and 2.12 injuries/1000 dance hours compared with 1.06 and 1.46 in the professional cohort, respectively (Smith et al, 2015). Of all injuries sustained in ballet, between 59%-93% are to the lower extremities (Bowerman Whatman, Harris, Bradshaw & Karin, 2014; Ramkumar, Farber, Arnouk, Varner & McCulloch, 2016), with the ankle reported to be the most commonly injured location (Smith et al, 2015).

The mechanism for ankle trauma typically involves an inverted and plantar-flexed foot configuration (Skazalski, Kruczynski, Bahr, Bere, Whiteley & Bahr, 2017), inherent to the multi-directional jump-landing manoeuvres performed repeatedly by dancers. Whilst the mechanism of injury is well corroborated, the aetiological understanding is incomplete given the multi-faceted nature of the associated risk factors. Of the numerous modifiable, intrinsic risk factors for injury, functional deficits in strength has been routinely purported. (Baumhauer, Alosa, Renstrom, Trevino & Beynnon, 1995; Murphy, Connolly & Beynnon, 2003; Willems, Witvrouw, Delabere, Mahieu, De Bourdeaudhuij & De Clercq, 2005). The strength of the peroneal musculature is integral to stabilising the ankle complex and may facilitate reduced risk of ligamentous injury by resisting coronal-plane forces (Fox, Docherty, Schrader & Applegate, 2008). The gold-standard measure of ankle strength involves isokinetic dynamometry, but previous assessments of isokinetic ankle strength in dancers have been restricted to plantar/dorsiflexion protocols (Thomas & Parcel, 2004; Schmitt, Kuni & Sabo, 2005; Kenne & Unnithan, 2008). Negating the inversion movement commonly associated with ankle injury mechanism, and the movement profile of dance, limits the functional relevance of previous applications which fail to inform the explicit strength training needs of dancers.

Isokinetic assessments of ankle eversion and inversion strength have been conducted on non-dance populations, utilising angular velocities of $30^{\circ}\cdot\text{sec}^{-1}$ and $120^{\circ}\cdot\text{sec}^{-1}$ (Willems, Witvrouw, Verstuyft, Vaes & De Clercq, 2002; Pontaga, 2004). These speeds appear to be selected arbitrarily to represent slow and fast motions, but without rationale provided by the authors. Isokinetic data collection is defined by predetermined selection of contraction mode, range of motion and angular velocity, which should reflect the specific research question. Contentious issues also surround data analysis with respect to the resultant metrics of strength that are assessed and quantified. Peak torque is typically the primary outcome measure from isokinetic assessments but provides only a single maximum value with little consideration of the entire strength curve. Arguably, strength deficits are of greater value for interventions targeting injury prevention or performance enhancement. Contemporary research (Eustace, Page & Greig, 2017) has advocated the inclusion of additional outcome measures including functional range and angle-specific derivatives of strength, assessed over a range of angular velocities.

The aim of the current study was to evaluate ankle evertor and invertor strength capacity in female ballet dancers across a range of functionally relevant joint angles and angular velocities.

151 Limb dominance was also considered given that a typical choreograph may contain up to 200
152 jumps, of which 56% involve one-footed landings (Liederbach, Dilgen & Rose, 2006). Further,
153 dancers may have a preferred limb for ‘pushing off’, jumping, or landing (Murphy, Connolly
154 & Beynon. 2003). The asymmetric movement sequence of a dance routine highlights the
155 importance of bilateral symmetry in the lower limbs to decrease the risk of injuries attributed
156 to compromised movement technique and posture (Croisier, Ganteaume, Binet, Genty &
157 Ferret, 2008, Fousekis, Tsepis & Vagenas, 2010; Menzel, Chagas, Szmuchrowski, Araujo, de
158 Andrade & de Jesus-Moraleida, 2013). A comprehensive profile of ankle eversion and
159 inversion strength that considers bilateral asymmetry in addition to ipsilateral mode and speed-
160 specific asymmetries, will inform clinical interpretation of the training needs required in this
161 cohort.

162

163 **2. Methods and Methods**

164

165 *2.1 Subjects*

166

167 A cohort of 14 female amateur ballet dancers (age: 19.29 ± 1.59 years; height: 1.65 ± 0.05
168 metres; body mass: 61.00 ± 8.29 kilograms) were recruited to participate in the study. A random
169 stratified sampling method was deployed to recruit participants from exiting institutional
170 undergraduate dance populations, indicating that all participants were aged 18+. Stringent
171 inclusion criteria dictated that participants were not dancing for a professional organisation.
172 Further, all dancers had a minimum of 8 years dancing experienced and were required to be
173 attending ballet training for a minimum of three hours per week. Participants were unable to
174 participate in the study if they had sustained an injury in the 3 months prior to their testing
175 session or were categorised as having ankle instability based on completion of the Cumberland
176 Ankle Instability Tool (CAIT) questionnaire. The current study was approved by the institute’s
177 departmental ethics committee, and, in accordance with the Declaration of Helsinki, all
178 participants obtained a study information sheet and provided written informed consent prior to
179 data collection.

180

181 *2.2 Procedures*

182

183 All participants were required to attend the Musculoskeletal Laboratory for one experimental
184 testing session. Participants initially completed a standardized warm-up targeting ankle joint
185 mobilisation. Ballet-specific exercises – 10 x Plié, 10 x Relevé (heel raise) – were completed
186 in accordance with the constructs of a warm-up preceding a typical ballet class, and were
187 followed by 10 slow eversion and inversion repetitions for both limbs (seated with legs
188 outstretched) in reference to the subsequent isokinetic protocol. Five sub-maximal (50% effort)
189 familiarisation trials of concentric ankle eversion (CON_{EV}) and inversion (CON_{INV}), and,
190 eccentric ankle inversion (ECC_{INV}) at all experimental testing velocities were completed as part
191 of the warm-up protocol. The familiarisation trials were completed with progressive increments
192 in angular velocity through the sequence; $30^{\circ}\cdot s^{-1}$, $60^{\circ}\cdot s^{-1}$, $90^{\circ}\cdot s^{-1}$, and $120^{\circ}\cdot s^{-1}$ for both limbs.
193 Experimental trials were subsequently completed following a five-minute rest period, with five
194 maximal repetitions for each contraction mode and speed.

195

196 *2.2.1 Isokinetic strength assessment*

197

198 Bilateral isokinetic ankle muscle strength was determined using an isokinetic dynamometer
199 (System 4 pro, Biodex Medical Systems, Shirley, New York, USA) following manufacturer-
200 recommended calibration. Each participant was asked to identify a preferred limb for which to

201 land on during a unilateral ballet-specific jump landing task, in accordance with previous
202 methods (Mertz and Docherty, 2012; Carcia, Cacolice & McGeary, 2019). For the purposes of
203 the current investigation, the preferred limb is classified as the dominant limb hereafter. Each
204 participant was positioned according to manufacturer's guidelines for ankle eversion/inversion
205 strength assessment (dynamometer orientation, 0°; dynamometer tilt, 50°; seat orientation 90°;
206 seatback tilt, 70°). A goniometer was used to set the foot attachment in 20° of plantarflexion to
207 partially replicate the orientation of the foot when landing from a jump during a dance routine.
208 Each participants' foot was secured to the ankle eversion/inversion footplate attachment using
209 Velcro straps, whilst an additional dynamometer attachment positioned at the mid portion of
210 the posterior thigh provided support to the testing limb. To further stabilize and isolate the
211 ankle joint, Velcro straps were also applied across the chest, and the mid portion of the anterior
212 thigh of the uninvolved limb. From a neutral position (vertical alignment of the foot), and to
213 standardize the test protocol for all participants, ankle eversion and inversion motion limits
214 were set at 20° resulting in an overall 40° range of motion.
215

216 Initiated at a position of max inversion (20°), all participants completed five maximal
217 concentric ankle eversion and inversion trials (Sekir, Yildiz, Hazneci, Ors & Aydin, 2007), at
218 angular velocities of 90°·s⁻¹, 60°·s⁻¹, 120°·s⁻¹ and 30°·s⁻¹ for both limbs, in accordance with
219 recommendations (Fish, Milligan & Killey, 2014). The non-linear order was chosen to
220 minimise any potential learning effect. The same procedure was then completed for the
221 eccentric ankle inversion trials. Concentric ankle eversion and inversion trials at each angular
222 velocity were interspersed with a one-minute rest period, whilst 10-minutes rest separated
223 ipsilateral concentric and eccentric trials to minimise the accumulation of fatigue (Yuksel,
224 Ozgurbuz, Ergun, Islegen, Taskiran, Deneral & Ertat, 2011). No performance feedback was
225 presented during any of the experimental trials.
226

227 *2.3 Data Processing*

228

229 Raw torque-angle time history data from each limb, contraction mode and angular velocity
230 were exported to Excel (Microsoft Corporation, Washington, USA) for further analysis. With
231 torque overshoot removed, the isokinetic phase of each repetition was determined, and the
232 repetition producing the highest torque was analysed. At each velocity and mode of contraction,
233 Peak Torque (PT), corresponding Angle of Peak Torque (APT), and Functional Range (FR –
234 defined as the range over which 85% of peak torque is maintained) were established. Angle-
235 Specific Torque (AST) data were calculated in 5° increments across the entire angular range
236 (40°) for all angular velocities and contraction modes. Corresponding Dynamic Control Ratios
237 (DCRs) were defined using PT (DCR_{PT}) and AST (DCR_{AST}) values.
238

239 *2.4 Statistical Analysis*

240

241 Descriptive statistics are presented as mean ± standard deviation (σ). The distribution of data
242 was quantified using histograms, Q-Q plots, skewness and kurtosis, and the Shapiro-Wilk
243 statistic. With the data normality assumption satisfied, linear mixed models were employed to
244 examine bilateral isokinetic strength differences in each outcome measure across all testing
245 velocities and contraction modes. Bonferroni-corrected post-hoc pairwise comparisons for
246 significant main effects and interactions were determined as required, and 95% confidence
247 intervals (CI) and Cohen's *d* effect sizes (small, 0.20-0.49; moderate, 0.50-0.79; large > 0.80)
248 were also presented. Alpha was determined a priori and deemed statistically significant at the
249 $p < 0.05$ level for all outcome measures. Statistical analyses were conducted using IBM SPSS
250 statistics V25.0 software (IBM, Armonk, New York, USA).

251 **3. Results**

252

253 *3.1 Peak torque*

254

255 Figure 1 summarises the influence of contraction mode and angular velocity on bilateral PT.
256 There was no significant main effect for limb ($p = 0.35$), nor any significant limb*contraction
257 mode ($p = 0.72$), limb*angular velocity ($p = 0.96$), or limb*contraction mode*angular velocity
258 ($p = 1.00$) interaction. Significant main effects for contraction mode ($p = 0.001$) and angular
259 velocity ($p = 0.001$) were identified, along with a significant contraction mode*angular velocity
260 interaction ($p = 0.001$). For instances where the main effect/interactions involving limb are not
261 significant, corresponding values for significant contraction mode, angular velocity and angle
262 main effects/interactions represent an average from the dominant and non-dominant limb and
263 this is consistent throughout. Figure 1 demonstrates that ECC_{INV} PT was significantly greater
264 than CON_{EV} and CON_{INV} at $60^\circ \cdot s^{-1}$ ($p = 0.001$, $d = 0.43-0.48$), $90^\circ \cdot s^{-1}$ ($p = 0.001$, $d = 0.67-$
265 0.73) and $120^\circ \cdot s^{-1}$ ($p = 0.001$, $d = 0.73-0.77$).

266

267

268 ****INSERT FIGURE 1 HERE****

269

270

271 *3.2 Angle of peak torque*

272

273 Table 1 displays bilateral APT data for all contraction modes and velocities. No significant
274 main effect for limb ($p = 0.82$) was obtained, nor was there any significant limb*contraction
275 mode ($p = 0.46$), limb*angular velocity ($p = 0.55$), or limb*contraction mode*angular velocity
276 ($p = 0.89$) interaction. Analyses revealed a significant main effect for contraction mode ($p =$
277 0.001) with ECC_{INV} APT ($27.10^\circ \pm 7.16^\circ$; CI: 25.83-28.50) occurring significantly later in the
278 range of motion compared with CON_{EV} ($18.45^\circ \pm 6.1^\circ$; CI: 17.20-19.70, $p = 0.001$, $d = 0.55$)
279 and CON_{INV} ($16.62^\circ \pm 6.46^\circ$; CI: 15.37-17.88, $p = 0.001$, $d = 0.61$) irrespective of angular
280 velocity. A significant main effect for angular velocity ($p = 0.02$) demonstrated that APT was
281 achieved significantly earlier at $30^\circ \cdot s^{-1}$ ($18.83^\circ \pm 9.03^\circ$, CI: 17.36-20.29) compared with $90^\circ \cdot s^{-1}$
282 ($22.17^\circ \pm 7.56^\circ$; CI: 20.70-23.63, $p = 0.01$, $d = 0.19$) irrespective of contraction type. No
283 significant contraction mode*angular velocity ($p = 0.27$) interaction was observed.

284

285

286 ****INSERT TABLE 1 HERE****

287

288

289 *3.3 Functional range*

290

291 Figure 2 illustrates the influence of contraction mode angular velocity on bilateral FR There
292 was no significant main effect for limb ($p = 0.10$), and no significant limb*contraction mode
293 ($p = 0.66$), limb*angular velocity ($p = 1.00$), or limb*contraction mode*angular velocity ($p =$
294 0.96) interaction. No significant main effect for contraction mode ($p = 0.15$) was found,
295 however a significant main effect for angular velocity ($F = 17.37$, $p = 0.001$) was revealed
296 irrespective of contraction mode. FR at $30^\circ \cdot s^{-1}$ ($18.67^\circ \pm 5.95^\circ$; CI: 17.56-19.79) was
297 significantly lower than at $60^\circ \cdot s^{-1}$ ($21.06^\circ \pm 5.01^\circ$; CI: 19.99-22.22; $p = 0.02$, $d = 0.20$) but
298 significantly higher compared with $120^\circ \cdot s^{-1}$ ($15.82^\circ \pm 6.27^\circ$; CI: 14.15-16.47; $p = 0.001$, $d =$
299 0.22). FR at $60^\circ \cdot s^{-1}$ was significantly greater than at $120^\circ \cdot s^{-1}$ ($p = 0.001$, $d = 0.41$), and at $90^\circ \cdot s^{-1}$
300 ($19.38^\circ \pm 5.35^\circ$; CI: 18.21-20.44) compared with $120^\circ \cdot s^{-1}$ ($p = 0.001$, $d = 0.29$). The significant

301 contraction mode*angular velocity interaction ($p = 0.001$) demonstrated that ECC_{INV} FR was
302 significantly greater at than CON_{EV} and CON_{INV} at $30^\circ \cdot s^{-1}$ ($p = 0.001$, $d = 0.46-0.57$), but
303 significantly lower at $120^\circ \cdot s^{-1}$ ($p = 0.001$, $d = 0.67-0.73$).
304
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307 *****INSERT FIGURE 2 HERE*****
308
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310 *3.4 Dynamic control ratios calculated from PT data.*

311

312 DCR_{PT} values are presented in Table 2. There was no significant main effect for limb ($p =$
313 0.90), nor a significant limb*contraction mode ($p = 0.15$), limb*angular velocity ($p = 0.75$)
314 0.05), or limb*contraction mode*angular velocity ($p = 0.98$) interaction. Significant main
315 effects for contraction mode ($p = 0.001$) and angular velocity ($p = 0.001$), and the
316 corresponding contraction mode*angular velocity interaction ($p = 0.01$) were highlighted.
317 There was no indication of any contraction mode*angular velocity interactions at $30^\circ \cdot s^{-1}$,
318 however $CON_{EV}:CON_{INV}$ dynamic control ratios were significantly greater than
319 $CON_{EV}:ECC_{INV}$ and $CON_{INV}:ECC_{INV}$ at $60^\circ \cdot s^{-1}$ ($p = 0.01$, $d = 0.38-0.49$), $90^\circ \cdot s^{-1}$ ($p = 0.001$, d
320 $= 0.70-0.77$) and $120^\circ \cdot s^{-1}$ ($p = 0.001$, $d = 0.74-0.78$) respectively.
321
322

323 *****INSERT TABLE 2 HERE*****
324
325

326 *3.5 Angle-specific Torque*

327

328 Figure 3 depicts the influence of contraction mode, angular velocity, and angle on bilateral
329 AST. There was no significant main effect for limb ($p = 0.59$), nor a significant interaction for
330 limb*contraction mode ($p = 0.86$), limb*angle ($p = 1.00$) limb*angular velocity ($p = 0.95$),
331 limb*contraction mode*angle ($p = 1.00$), limb*contraction mode*angular velocity ($p = 0.68$),
332 limb*angle*angular velocity ($p = 1.00$), or limb*contraction mode*angle*angular velocity (p
333 $= 1.00$) interaction. Significant main effects for contraction mode ($p = 0.001$), angle ($p = 0.001$),
334 and angular velocity ($p = 0.001$), and, significant contraction mode*angle ($p = 0.001$), and
335 contraction mode*angular velocity ($p = 0.001$) were identified. Analyses revealed that ECC_{INV}
336 torque was significantly greater than the two concentric modes for angles $\geq 15^\circ$ during the
337 $30^\circ \cdot s^{-1}$, $60^\circ \cdot s^{-1}$ and $90^\circ \cdot s^{-1}$ trials, and for angles $\geq 25^\circ$ during $120^\circ \cdot s^{-1}$ (see figure 3).
338
339

340 *****INSERT FIGURE 3 HERE*****
341
342

343 *3.6 Dynamic control ratios derived from AST data.*

344

345 Table 3 summarises the effect of angle and angular velocity on the respective bilateral DCR_{AST}.
346 There was no significant main effect for limb ($p = 0.58$), nor a significant limb *contraction
347 mode ($p = 0.08$), limb*angle ($p = 1.00$), limb*angular velocity ($p = 0.17$), limb*contraction
348 mode*angle ($p = 1.00$), limb*contraction mode*angular velocity ($p = 0.47$),
349 limb*angle*angular velocity ($p = 1.00$), or limb*contraction*mode*angle*angular velocity (p
350 $= 1.00$) interaction. However, significant main effects for contraction mode ($p = 0.001$), angle

351 (p = 0.01) and angular velocity (p = 0.001) were identified, along with a significant contraction
352 mode*angle (p = 0.001) and contraction mode*angular velocity (p = 0.02) interaction. At
353 angles $\geq 15^\circ$, CON_{EV}:CON_{INV} dynamic control ratios were significantly higher than
354 CON_{EV}:ECC_{INV} and CON_{INV}:ECC_{INV}. Moreover, CON_{EV}:CON_{INV} dynamic control ratios were
355 also significantly greater than the ECC_{INV}-inclusive ratios at all isokinetic speeds (see table 3).
356 There was no significant angle*angular velocity (p = 0.59) or contraction mode*angle*angular
357 velocity (p = 0.97) interaction.

358
359
360 *****INSERT TABLE 3 HERE*****
361

362 4. Discussion

363
364 Strength deficits have been implicated as a modifiable risk factor for ankle injury, a prevalent
365 injury in ballet (Willems et al, 2005; Smith et al, 2015). Contrary to previous research, the
366 present study focused strength profiling on the ankle eversion/inversion mechanism that is
367 fundamental to the physical demands of ballet and the common mechanism of injury. Main
368 effects for limb dominance were investigated for all isokinetic outcome measures in
369 consideration of the aesthetic demand for movement symmetry within choreographed routines.
370 There was no evidence of bilateral asymmetry in any of the isokinetic ankle strength measures.
371 During a dance choreograph, a performer is presumed to execute technical intricacies using
372 each leg equally, and therefore, technique/rehearsal classes are assumed to facilitate bilateral
373 development (Farrar-Baker & Wilmerding, 2006). A key responsibility for the ankle joint is to
374 attenuate resultant mechanical loads following contact with the ground, to which strength plays
375 a pivotal role. With over half of jumps during a typical routine requiring a unilateral landing
376 component (Mertz & Docherty, 2012), symmetry between limbs is desirable to minimise a
377 greater loading and ensuing tendency to sustain injury in a particular side. The symmetry in
378 isokinetic strength in this population may be attributed to an early emphasis on bilateral limb
379 control in dance training, which may be crucial in developing equal bilateral strength, and
380 reducing ankle injury risk (Bronner & Ojofeitimi, 2006). Dance injury epidemiology literature
381 is not available to critically discuss this finding in relation to injury risk, however bilateral and
382 ipsilateral isokinetic strength discrepancies have been associated with an increased injury risk
383 (Croisier et al, 2008).

384
385 Potential strength imbalances were also considered in respect to contraction mode and
386 movement speed. The contraction mode*angular velocity interaction demonstrated that
387 ECC_{INV} strength was significantly greater than CON_{EV} and CON_{INV} at all but the slowest
388 angular velocity, with implications for DCRs. This observation is consistent with the classic
389 force-velocity profile comprising each contraction type, in that concentric strength typically
390 reduces as a product of increasing angular velocity, whereas eccentric strength remains
391 relatively constant (Cress, Peters & Chandler, 1992). The higher values observed for ECC_{INV}
392 strength at the greater angular velocities – which arguably have better functional relevance with
393 regards to dance performance - may be crucial in preventing the inverted foot alignment
394 mechanism common to ankle sprain incidence (Kaminski, Buckley, Powers, Hubbard & Ortiz,
395 2003).

396
397 The FR metric provides insight on the profile of the strength curve, with higher values
398 indicative of the ability to maintain >85% of PT for a greater range of motion. In this study,
399 FR was defined at 85% of PT based on observations that a 15% reduction in PT increases injury
400 risk (Croisier et al, 2008). Although this data is not available in a dance population,

401 consideration of the FR metric in isokinetic strength analyses may prove vital in identifying
402 markers for injury. At the slower velocities ($30^{\circ}\cdot s^{-1}$ and $60^{\circ}\cdot s^{-1}$), ECC_{INV} FR was higher than
403 both concentric modes. However, an inverse trend was established in the contraction
404 mode*angular velocity interaction at faster velocities ($90^{\circ}\cdot s^{-1}$ and $120^{\circ}\cdot s^{-1}$), whereby CON_{EV}
405 and CON_{INV} FR decreased marginally relative to the significant reductions demonstrated for
406 ECC_{INV} . In accordance with ankle injury aetiology (Skazalski et al, 2017) and the performance
407 characteristics of dance (Twitchett, Koutedakis & Wyon, 2009), the notable decline in ECC_{INV}
408 FR at higher velocities may have implications on injury susceptibility when executing dance-
409 specific locomotion. Lower ECC_{INV} strength may compromise the ability to resist inversion
410 forces thereby proliferating injury risk (Fox et al, 2008). Rather than using PT – which provides
411 a single strength value for a pre-determined range of motion – in the pursuit of identifying
412 markers for injury, professionals with an injury reduction focus may benefit from the FR metric
413 during isokinetic strength testing. The significant reductions in ECC_{INV} FR at angular velocities
414 exceeding $60^{\circ}\cdot s^{-1}$ provides a focus for subsequent strength training interventions. Even if PT
415 and the maxima of strength curve is unchanged, a reduction in FR suggests a decrease in
416 strength away from the single joint angle defined as APT. Practically, a dancer would benefit
417 from high PT and FR since performance demands will move through an angular range at the
418 ankle. However, it should be acknowledged that a decrease in FR across all contraction modes
419 at higher velocities may be indicative of a limited isokinetic phase as the dynamometer crank
420 arm accelerates to higher speeds over a relatively small range of motion. Torque may indeed
421 be maintained at 85% of PT outside the isokinetic range, but the restricted focus on the
422 isokinetic data curtails the FR metric. The range of movement for ankle eversion and inversion
423 is smaller than knee flexion/extension for example (Eustace et al, 2017), and thus, FR values
424 appear to be joint specific and should be interpreted with this in mind. Moreover, direct
425 comparisons of FR between relevant studies may only be achievable when uniform
426 methodological designs are used.

427
428 Conventional DCRs are derived from PT values without any consideration of the angle at
429 which PT is achieved, and thus, limit an understanding of how strength changes as a function
430 of angle. Data from the current investigation demonstrated that Peak CON_{EV} and CON_{INV}
431 torque was achieved at $\sim 18^{\circ}$ (2° of inversion) and $\sim 17^{\circ}$ (3° of eversion), thereby representing
432 a relatively neutral foot alignment over the 40° range of motion. ECC_{INV} PT occurred
433 significantly later at $\sim 27^{\circ}$, representing a 7° position of inversion. Previous literature has failed
434 to quantify the angle of peak torque for ankle inversion/eversion isokinetic strength ratios,
435 preventing direct comparison. However, studies examining strength parameters at the knee
436 joint have demonstrated that APT varies between concentric and eccentric modes of
437 contraction and across a range of angular velocities (Cohen, Zhao, Okwera, Matthews &
438 Delextrat, 2015; Eustace et al, 2017). The evident inconsistencies for APT from the current
439 study and indeed other investigations, raises questions over the value of traditional PT-derived
440 strength ratios and supports the inclusion of AST assessed across a number of angular
441 velocities. The greater PT but smaller FR in ECC_{INV} at higher velocities has implications for
442 functional performance and the strategies deployed in training and/or rehabilitation. The
443 inverted configuration in ECC_{INV} – approximately 7° – compared with concentric modes may
444 serve as a protective mechanism against ankle injury during execution of dance-specific
445 movement, in which the foot is frequently loaded into inversion (O’Loughlin, Hodgkins &
446 Kennedy, 2008).

447
448 Findings from the study revealed significant main effects for contraction mode, angle, and
449 angular velocity on AST, whilst significant contraction mode*angle and contraction
450 mode*angular velocity interactions were also revealed. Data for AST and corresponding

451 controls ratios were significantly higher for ECC_{INV} than CON_{EV} and CON_{INV}, with more
452 profound differences observed at the latter ranges of the movement, and with increasing
453 angular velocity. This finding may be attributed to both the force-velocity and force-angle
454 relationships between contraction modes. CON_{EV} and CON_{INV} strength portray a quadratic
455 trend, in which PT is achieved at approximately midpoint of the movement, whereas ECC_{INV}
456 PT is achieved towards end range. The use of angle-specific torque is sensitive to the changes
457 in strength at various positions within a movement. Resultant DCRs may be used in the
458 screening of performers towards injury reduction, and in the management of injury during
459 rehabilitation. For example, in the current study, whilst decreases in CON_{INV} strength near to
460 full ankle inversion were exacerbated as angular velocity increased, ECC_{INV} was relatively
461 consistent. ECC_{INV} dominance at the end ranges of movement and at higher velocities may
462 indeed reduce the likelihood of ankle injury when executing the jump-landing, cutting
463 manoeuvres of a dance routine.

464
465 Caution ought to be taken when generalising these findings beyond the specific experimental
466 design employed. Isokinetic testing protocols have some inherent methodological constraints,
467 which should be considered when developing the data collection paradigm. The joint range of
468 motion and joint angular velocities used in the current study are close to the physiological
469 capabilities of the ankle when tested in this restricted state. Pilot testing highlighted that no
470 isokinetic phase was determined at angular velocities of $\geq 150^{\circ}\cdot s^{-1}$, and the range of motion is
471 prescribed using passive movement of the joint. Consequently, this passive manipulation of the
472 joint within an isokinetic testing paradigm may not reflect the physical capacity of the joint
473 during active movement. In the current investigation, limb dominance was determined using a
474 prospective classification based on preference to ballet-specific tasks. Carcia et al. (2019)
475 highlighted that limb dominance was task-specific, and thus, our approach is specific to the
476 participants and focus of our study. The use of alternative classifications of limb dominance,
477 including retrospective classification based on outcome measures, and the impact on
478 interpretation of the findings warrants future research. The present study focused on ankle
479 eversion/inversion strength given its mechanical associations with injury. However, a strength
480 profile of dancers may include plantar/dorsiflexion strength in light of kinematic analyses
481 highlighting ankle injuries to occur in neutral (Fong, Chan, Mok, Yung, & Chan, 2009) and
482 dorsi-flexed positions (Kristianslund, Bahr, & Krosshaug, 2011). Kinematic analyses of injury
483 incidence or dance-specific movements may inform bespoke isokinetic testing protocols but
484 must also account for physical limitations of the ankle during such assessments. Further
485 research is required in the associations between isokinetic metrics and injury incidence, which
486 may inform a threshold for the calculation of FR. Contemporary analysis metrics that delve
487 beyond the highest value of a strength curve are advocated. Data collection ought to utilise the
488 capacity of the isokinetic dynamometer to measure net joint torque at predetermined angles
489 and angular velocities to provide a screening battery of greatest functional relevance to the
490 sport.

491 492 **5. Conclusions**

493
494 This is the first study to consider the eversion/inversion strength of female ballet dancers, with
495 previous literature considering only plantar/dorsiflexion despite the influence of inversion on
496 ankle injury mechanics. Findings from the current study demonstrate bilateral symmetry in
497 female dancers during a comprehensive isokinetic ankle strength testing protocol. This
498 observation may be attributed to both appropriate training interventions from an early age, and,
499 regular exposure to the asymmetric movement patterns of dance that facilitates bilateral
500 development. The isokinetic strength profile of dancers in this study illustrated that ECC_{INV}

501 strength is maintained over a range of angular velocities, compared with reductions in CON_{EV}
502 and CON_{INV} strength as movement speed increases. Specifically, dancers appear to be ECC_{INV}
503 dominant at angular velocities of 60°·s⁻¹ and beyond, and for all angular displacements
504 providing implications for functional performance and injury risk. Beyond the singular peak of
505 the torque-angle curve, ECC_{INV} had greater FR at velocities <90°·s⁻¹ compared with the
506 concentric modes, which may indicate a protective mechanism for injury. The results and
507 methods highlighted within this study provide medical practitioners with the opportunity to
508 produce a comprehensive isokinetic strength profile of dancers. This information can be used
509 to help enhance understanding of injury occurrence, whilst producing more detailed
510 information for a dancers return to performance.

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513 **Ethical approval**

514 Approval of this study was granted by the University's departmental ethics committee.

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517 **Disclosure of interest**

518 The authors report no conflict of interest.

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634 **Legend to Tables and Figures**

636

637 *Tables*

638

639 **Table 1.** The influence of angular velocity, limb and mode of contraction on APT.

640

641 **Table 2.** The influence of limb and angular velocity on selected Dynamic Control Ratios
642 calculated from PT. Values are mean \pm σ .

643

644 **Table 3.** The influence of limb, angle and angular velocity on the corresponding DCR_{AST} data.
645 Values are mean \pm σ .

646

647 *Figures*

648

649 **Figure 1.** PT for each mode of contraction for the dominant (top) and non-dominant (bottom)
650 limb. Values are mean \pm σ . * denotes a significant difference between the eccentric and
651 concentric-inclusive contraction modes.

652

653 **Figure 2.** FR for each mode of contraction for the dominant (top) and non-dominant (bottom)
654 limb. Values are mean \pm σ . * denotes a significant difference between the eccentric and
655 concentric-inclusive contraction modes.

656

657 **Figure 3.** Angle-specific torque for each mode of contraction for the dominant (left) and non-
658 dominant (right) limb. Values are mean \pm σ . * denotes a significant difference for AST between
659 the eccentric and concentric-inclusive contraction modes.

660

661